

1 ASSEMBLY FOR SEALING AND CENTERING IN A TWO-CYLINDER DASHPOT OR
2 TWO-CYLINDER TELESCOPING LEG

3 The present invention concerns an assembly for sealing and
4 centering a piston rod in a two-cylinder dashpot or two-cylinder
5 telescoping leg as recited in Claim 1.

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7 In a two-cylinder dashpot, a piston rides up and down on the
8 inside end of a piston rod that travels into and out of an inner
9 cylinder. The piston rests more or less tight against the inner
10 surface of the cylinder, demarcating a fluid-filled compression
11 chamber. The fluid absorbs the incoming shock. An accommodation
12 in the form of a cushion of gas at the top of the gap between the
13 two cylinders compensates for the varying volume of the piston
14 rod as it travels in and out.

15
16 To ensure reliable and smooth shock absorption, especially when
17 the piston rod is moving very rapidly, the shock-absorbing fluid
18 is generally supplied compressed. Pressures of 3 to 8 bars are
19 normal.

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21 A component called a piston-rod sealing-and-centering assembly is
22 provided at the top of the overall device to radially position
23 the piston rod in relation to the inner and outer cylinders and
24 to seal it off from the environment. This assembly comprises an
25 outward-facing piston-rod sealing ring and an inward-facing

1 piston-rod centering ring resting against the inward-facing face
2 of the sealing ring.

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4 Gas, however, can leak out of the gas accommodation into the
5 inner cylinder's chambers. A checkvalve is accordingly provided
6 between the piston-rod centering ring and the piston-rod sealing
7 ring, communicating with the gas accommodation to allow the
8 escaped material to return therein.

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10 A piston-rod sealing-and-centering assembly of this genus is
11 known from German 2 832 640 A1. It entails the drawback, however,
12 that the situation of the checkvalve between the piston rod and
13 the gas accommodation considerably complicates the design.

14 Another drawback is that the "high-pressure sealing ring" between
15 the piston-rod centering ring and the piston-rod sealing ring is
16 in contact with the rod and accordingly causes friction.

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18 One object of the present invention is accordingly components of
19 a piston-rod sealing-and-centering assembly of the aforesaid
20 genus designed and arranged to eliminate the need for a high-
21 pressure sealing ring in contact with the piston rod. Another
22 object is a simpler checkvalve in the overflow channel.

23

24 This object is attained in accordance with the present invention
25 in a piston-rod sealing-and-centering assembly with the

1 characteristics recited in Claim 1. Alternative and advanced
2 embodiments are addressed by Claims 2 through 4.

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4 The advantages of the present invention derive in particular from
5 the low-friction and wear-resistant material employed for the
6 piston-rod sealing ring. The piston-rod sealing ring can
7 accordingly be unobjectionably subjected to high pressure just
8 during the decompression phase, eliminating the need for a
9 particularly high-pressure tightness between the cylinder and the
10 piston-rod sealing ring. This approach will considerably decrease
11 the friction between the piston-rod sealing ring and the piston
12 rod and hence the dashpot's tendency to stick and slip.

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14 One embodiment of the present invention will now be specified
15 with reference to the attached drawing, wherein

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17 Figure 1 is a section through the vicinity of a piston-rod
18 sealing-and-centering assembly in a two-cylinder dashpot,

19

20 and

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22 Figure 2 a larger-scale section through half of the piston-rod
23 sealing-and-centering assembly depicted in Figure 1.

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25 The housing of a two-cylinder dashpot or telescoping leg (whereby

1 the former term shall be understood to refer to either device
2 hereinafter) comprises two co-axial cylinders, an outer cylinder
3 1 and an inner cylinder 2. A piston rod 3 travels into and out of
4 the housing through its top, which is open. Mounted on the end of
5 piston rod 3 inside the housing is an unillustrated piston that
6 rests against the inner surface of inner cylinder 2, demarcating
7 a fluid-filled pressure-application chamber 4 and generating the
8 shock-absorbing force by way of valve-controlled ports.

9
10 The moving piston rod 3 is sealed off from and centered in
11 relation to the housing by a piston-rod sealing-and-centering
12 assembly 5. The assembly illustrated in Figures 1 and 2
13 essentially comprises a piston-rod centering ring 6 and a piston
14 rod sealing ring 7 in the form of a gasket. The wall of piston-
15 rod centering ring 6 is approximately Z-shaped in cross-section.
16 At upper end 8, it rests with its outside circumference against
17 the inner surface of outer cylinder 1, decreases at a midpoint 9
18 to form a more or less sleeve-like structure with an inner
19 circumference approximately matching the diameter of piston rod
20 3, and extends axially inward at lower end 10, its outer
21 circumference resting against the inner surface of inner cylinder
22 2. Mounted on the inner surface of the piston-rod centering ring
23 6 in the illustrated example is a bushing 11 that radially
24 secures piston rod. It would alternatively be conceivable for
25 piston rod 3 to rest radially directly against the inner surface

1 of piston-rod centering ring 6.
2
3 Piston-rod sealing ring 7 fits into a flowerpot-shaped
4 accommodation at the upper end 8 of piston-rod centering ring 6.
5 The inner surface of piston-rod sealing ring 7 is provided with a
6 radially inward open groove 12 accommodating a multiple-part seal
7 13 that seals off sealing-and-centering assembly 5 and hence the
8 dashpot housing from piston rod 3. Another seal, seal 14, seals
9 off sealing-and-centering assembly 5 from outer cylinder 1, which
10 is upset at its upper end to axially secure the dashpot's
11 components.
12
13 A venting system is illustrated in larger scale in Figure 2. The
14 outer circumference of the base of the flowerpot-shaped
15 accommodation is provided with a continuous groove 15 that can
16 accommodate a special seal 16. The main cross-section of seal 16
17 is round, and the seal is provided with a lip 17 that extends
18 radially outward at the bottom. Unstressed, lip 17 rests against
19 a conical surface 18 of groove 15. Seal 16 is inserted with its
20 main cross-section in the groove between piston-rod centering
21 ring 6 and piston-rod sealing ring 7. Various channels that will
22 be specified in greater detail hereinafter act as venting
23 components that create a one-way communication between the
24 section between sliding bushing 11 and seal 13 on the one hand
25 and a gas accommodating space 19 on the other. Gas-accommodating

1 space 19 is at the top of the gap between inner cylinder 2 and
2 outer cylinder 1. Below it, and in pressure-application chamber 4
3 as well, is shock-absorbing fluid.
4
5 Any bubbles of gas or leaking oil between bushing 11 and seal 13
6 will be conveyed to gas-accommodating space 19 through a series
7 of channels. This system consists essentially of channels 20, 21,
8 and 22 that extend radially from the inner surface to the outer
9 surface of piston-rod centering ring 6. They extend, open at the
10 top, either along the base of the accommodation in piston-rod
11 centering ring 6 that accepts piston-rod sealing ring 7 or along
12 the base of groove 15 below the main cross-section of seal 16.
13 Channel 22 no longer extends into the conical surface 18 that lip
14 17 rests against. Groove 15 communicates with gas-accommodating
15 space 19 through local apertures 23.
16
17 As will be evident from Figure 2, lip 17 acts in conjunction with
18 conical surface 18 as a checkvalve, preventing the gas in gas
19 accommodating space 19 from penetrating between bushing 11 and
20 seal 13.
21
22 The resilience and shape of lip 17 provide, along with variations
23 in the dimensions and number of radial channels 20, 21, and 22,
24 simple means of adjusting the performance of the venting system
25 to various needs. The diaphragm effect provided by the channel 22

1 below seal 16 in particular ensures that the performance will be
2 constant independent of manufacturing tolerances.

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